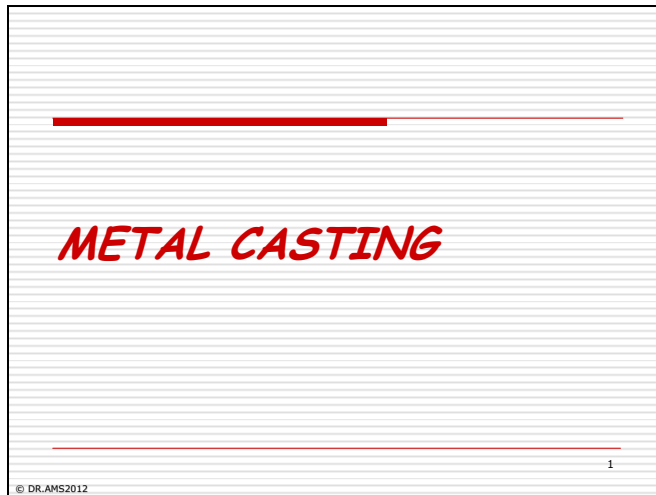
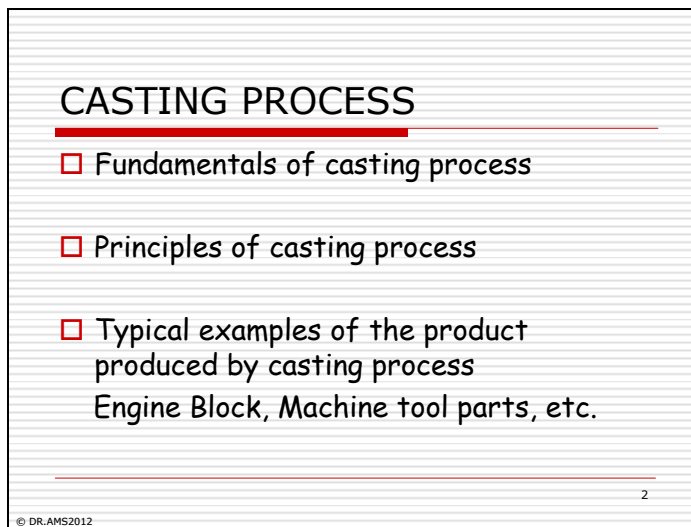


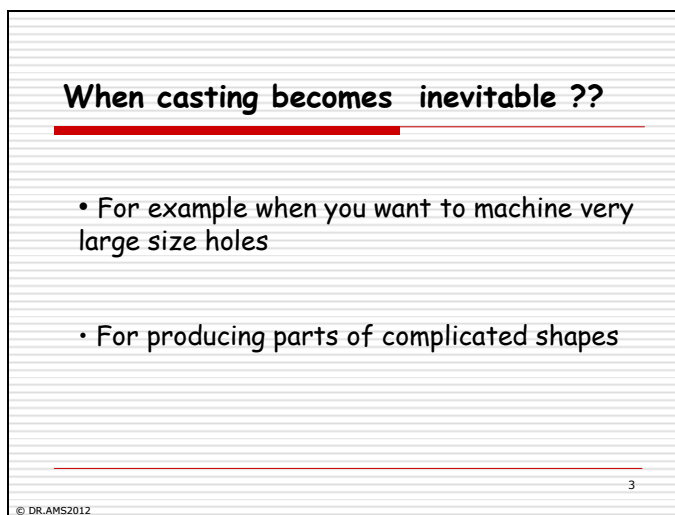
Slide 1



Slide 2



Slide 3



Slide 4

CASTING PROCESS

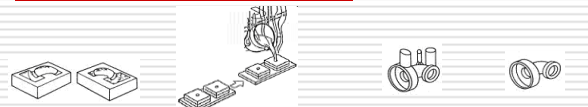
- ❑ Steps involved in casting process
 - ❑ Pattern making.
 - ❑ Mould making.
 - ❑ Core making.
 - ❑ Melting of metal and pouring.
 - ❑ Cooling and solidification
 - ❑ Cleaning of castings and inspection

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Slide 5

Casting



Refractory mold → pour liquid metal → solidify, remove → finish

- **VERSATILE:** complex geometry, internal cavities, hollow sections
- **VERSATILE:** small (~10 grams) → very large parts (~1000 Kg)
- **ECONOMICAL:** little wastage (extra metal is re-used)
- **ISOTROPIC:** cast parts have same properties along all directions

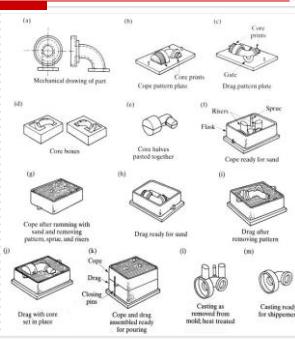
5

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Slide 6

Sand Casting

- Cope:** Top half
- Dag:** Bottom half
- Core:** for internal cavities
- Pattern:** positive
- Funnel → sprue → runners → gate → cavity → {risers, vents}**



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Slide 7

Sand Casting Considerations

(a) How do we make the **pattern**?

[cut, carve, machine]

(b) Why is the pattern not exactly identical to the part shape?

- pattern → outer surfaces; (inner surfaces: core)
- shrinkage, post-processing

(c) **parting line**

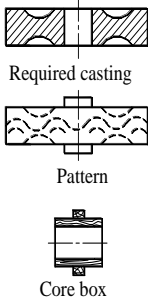
- how to determine?

7

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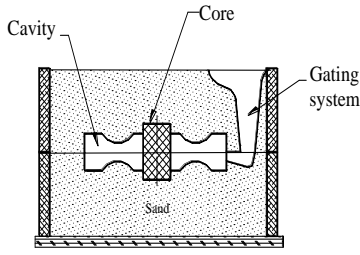
CASTING PROCESS



Required casting

Pattern

Core box



Cavity

Core

Sand

Gating system

Sand mould in two-piece flask

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Slide 9

Sand Casting Considerations..

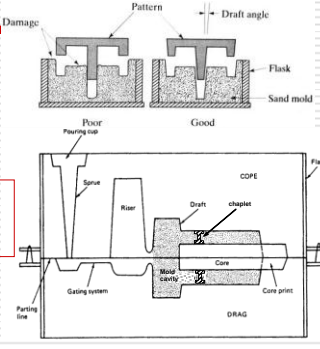
(d) **taper**

- do we need it ?

(e) **core prints, chaplets**

- hold the core in position
- chaplet is metal (why?)

(f) **cut-off, finishing**



Damage

Pattern

Draft angle

Flask

Sand mould

Pour

Pouring top

Good

Flask

COPE

Flask

Riser

Draft

chaplet

Core

Core print

DRAG

Parting line

Gating system

Flask cavity

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Slide 10

PROPERTIES OF PATTERN MATERIAL ...

- It should be easily shaped, worked, machined and joined.
- It should be resistant to wear and corrosion.
- It should be resistant to chemical action.
- It should be dimensionally stable and must remain unaffected by variations in temperature and humidity.
- It should be easily available and economical.

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WOOD

- Easily available
- Low weight
- Low cost
- It absorbs moisture and hence dimensions will change
- Lower life
- Suitable for small quantity production and very large size castings.

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METAL

- Used for mass production
- For maintaining closer dimensional tolerances on casting.
- More life when compared to wooden patterns
- Few of the material used include CI, Al, Fe, Brass etc. Al is widely used.

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Slide 13

PLASTIC

- ❑ Low weight
- ❑ Easier formability
- ❑ Do not absorb moisture
- ❑ Good corrosion resistance

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POLYSTYRENE

- ❑ Used for prototype (single piece) castings
- ❑ Also known as Disposable patterns.

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TYPES OF PATTERNS

The diagram shows three types of patterns used in casting:

- (a) Solid pattern: A single, solid block with a cavity, shown in a cross-section and a perspective view.
- (b) Split pattern: A pattern divided into two parts, labeled 'Part 1' and 'Part 2', held together by a 'Dowel pin'.
- (c) Loose piece pattern: A pattern made of several separate pieces, labeled 'Loose pieces', which are assembled to form the desired shape.

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TYPES OF PATTERNS

- ❖ **SOLID PATTERN**
Simple shape castings are produced by this type of patterns

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TYPES OF PATTERNS

- ❖ **SPLIT PATTERN**
Used when patterns cannot be made as a single piece

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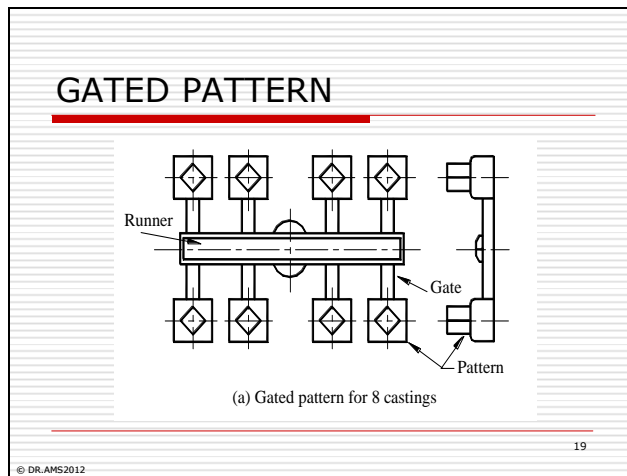
Slide 18

TYPES OF PATTERN

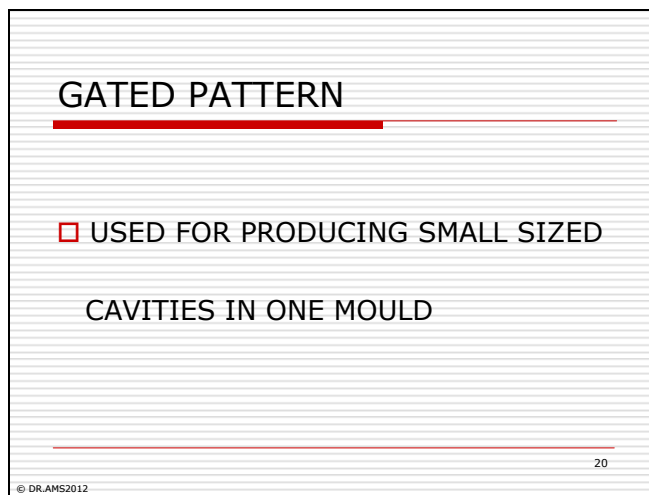
- **LOOSE PIECE PATTERN** Used when
 1. Withdrawal of pattern from mould is not possible
 2. Castings is having projections, undercuts, etcAfter ramming first main pattern is removed and then the loose pieces

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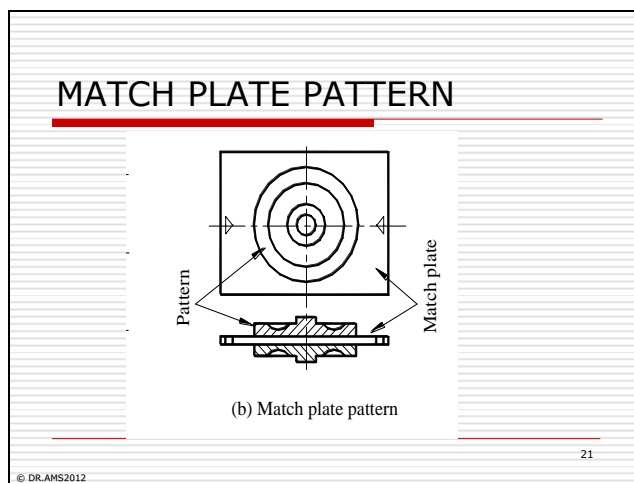
Slide 19



Slide 20



Slide 21



Slide 22

MATCH PLATE PATTERN

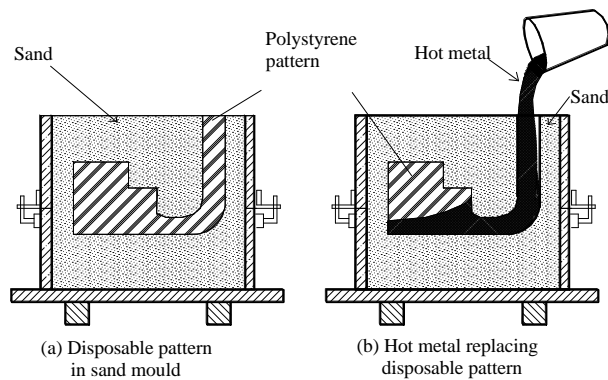
- Split patterns attached on either side is known as *Match plate pattern*.
- It increases production and helps in maintaining uniformity in the size and shape of the castings.

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DISPOSABLE PATTERN



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PATTERN ALLOWANCE

- WHY ARE ALLOWANCES NECESSARY ?

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TYPES OF ALLOWANCE

- ❑ SHRINKAGE ALLOWANCE
- ❑ MACHINING ALLOWANCE
- ❑ DRAFT OR TAPER ALLOWANCE
- ❑ DISTORTION ALLOWANCE
- ❑ RAPPING OR SHAKE ALLOWANCE

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SHRINKAGE ALLOWANCE

- Provided to compensate for shrinkage of material
- Pattern is made slightly bigger
- Amount of allowance depends upon type of material, its composition, pouring temperature etc.

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MACHINING ALLOWANCE

- Provided to compensate for machining on casting.
- Pattern is made slightly bigger is size.
- Amount of allowance depends upon size and shape of casting, type of material, machining process to be used, degree of accuracy and surface finish required etc.

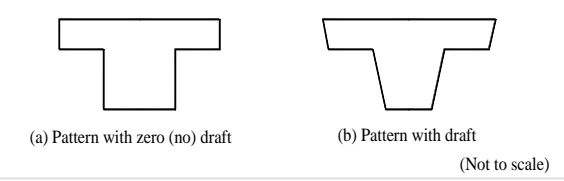
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DRAFT OR TAPER ALLOWANCE

(a) Pattern with zero or no draft (b) Pattern with draft



(a) Pattern with zero (no) draft (b) Pattern with draft
(Not to scale)

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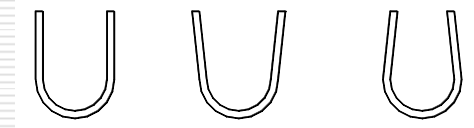
DRAFT OR TAPER ALLOWANCE

- Provided to facilitate easy withdrawal of the pattern.
- Typically it ranges from 1 degree to 3 degree for wooden patterns.

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DISTORTION ALLOWANCE



(a) Required shape of casting (b) Casting produced when no distortion allowance is provided (c) Pattern with distortion allowance

- Provided on patterns whose castings tend to distort on cooling

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MOULDING PROCESS

- Bench Moulding
- Floor Moulding
- Pit Moulding

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TYPES OF MOULDING OPERATIONS

- Hand Moulding
- Machine Moulding

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CORES

- Why Cores are used?**

The diagram illustrates the components and setup for sand casting with a core. On the left, it shows the 'Required casting' (a cross-section of a part with a central hole), the 'Pattern' (a cross-section of the mold), and the 'Core box' (a container for the core). On the right, it shows the 'Sand mould in two-piece flask' (a cross-section of the mold assembly). The flask contains 'Sand', a 'Core' (a central part), and a 'Gating system' (a channel for the molten metal).

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CORE PROPERTIES

- ❑ It must be strong to retain the shape while handling,
- ❑ It must resist erosion by molten metal,
- ❑ It must be permeable to gases,
- ❑ It must have high refractoriness, and
- ❑ It must have good surface finish to replicate it on to the casting.

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STEPS IN CORE MAKING

- ❑ Core sand preparation.
- ❑ Core making.
- ❑ Core baking.

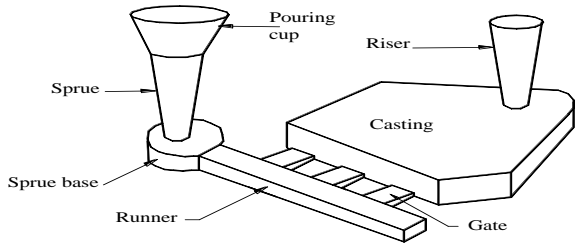
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GATING SYSTEM

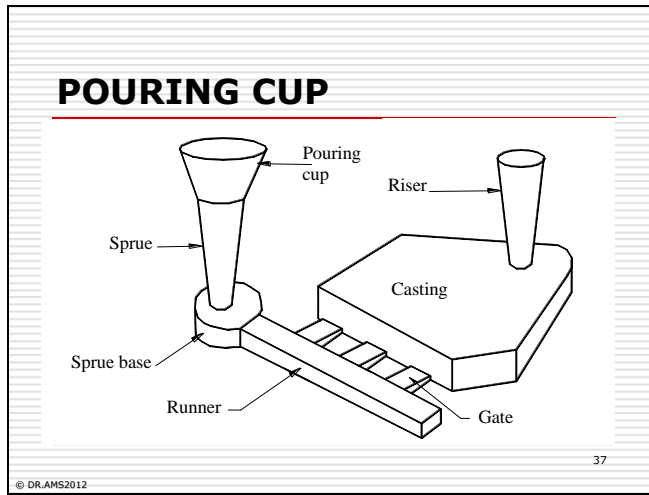
- ❑ It refers to the passageway through which molten metal passes to enter mould cavity.



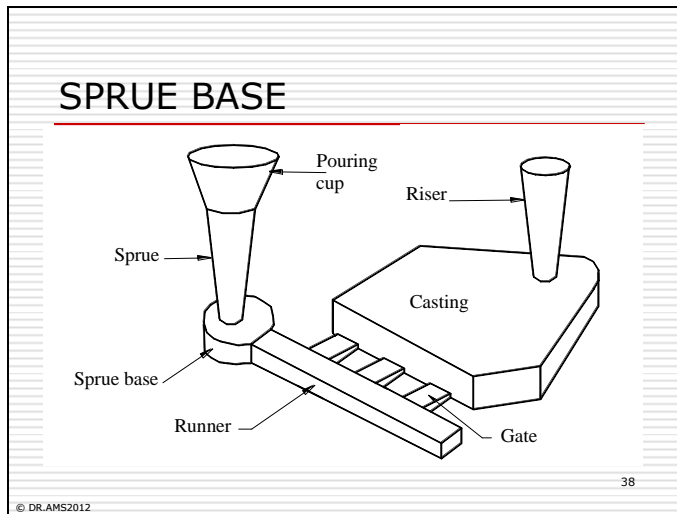
The diagram illustrates a gating system for a casting. It shows a pouring cup at the top left, which leads to a sprue. The sprue is supported by a sprue base. From the bottom of the sprue, a runner extends to the right, leading to a gate. The gate is the opening through which molten metal enters the casting mold. The casting is shown as a rectangular block on the right. A riser is also shown, which is a reservoir of molten metal that feeds the casting as it shrinks during solidification.

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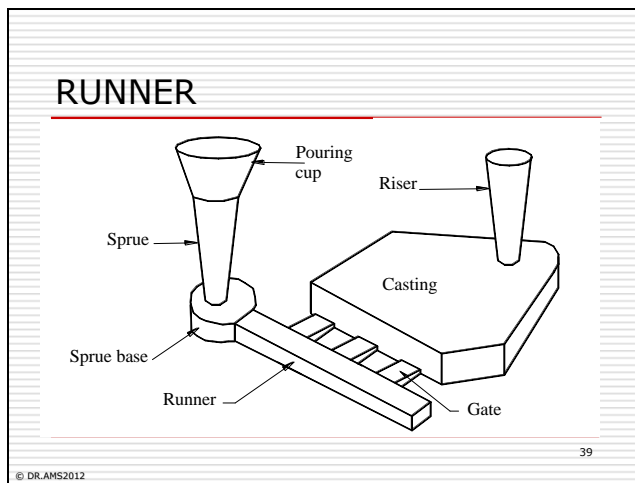
Slide 37



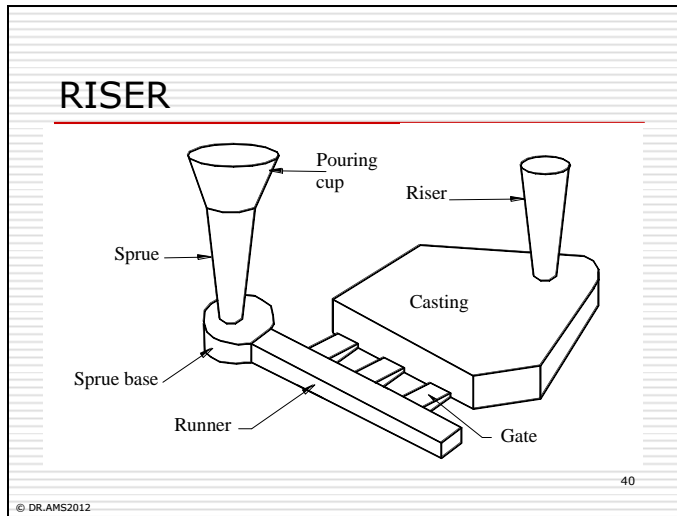
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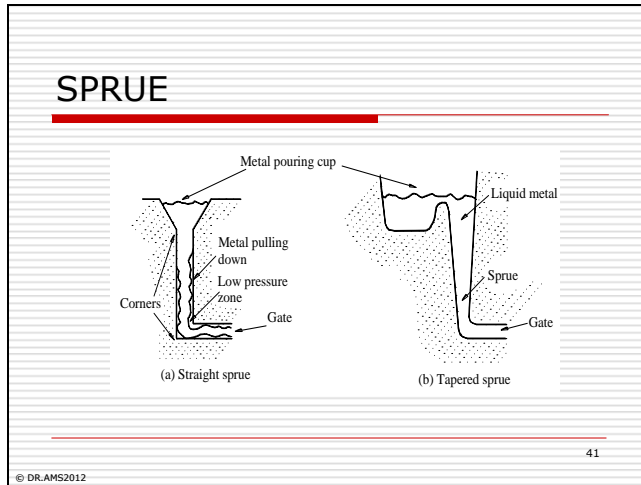
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Slide 40



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SOLIDIFICATION TIME

[Chvorinov's Rule]

□ Total Solidification Time[TST]

$$TST = c \left(\frac{\text{volume}}{\text{surface area}} \right)^n$$

Where c = mould constant depends upon the mould material, metal properties & temperature

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Mold Constant in Chvorinov's Rule

- C_m depends on mold material, thermal properties of casting metal, and pouring temperature relative to melting point
- Value of C_m for a given casting operation can be based on experimental data from previous operations carried out using same mold material, metal, and pouring temperature, even though the shape of the part may be quite different

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CASTING YIELD

- What is casting yield?

$$C_y = \frac{W_c}{W_c + W_g} \times 100\%$$

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DEFECTS IN CASTING

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Basic categories of casting defects

1. Metallic projections:
 - Fins, flash or projections
2. Cavities
 - blow holes, pin holes, shrinkage cavities
3. Discontinuities
 - cracks, cold or hot tears
 - cold shuts- improper fusion of different streams of metals
 - Improper solidification can cause tears

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4. Defective surface
 - Surface folds ,laps, scars, adhering sand layers and oxide scales
5. Incomplete casting
 - misruns (due to premature solidifications)
 - insufficient metal poured
 - leaks in the mold
6. Incorrect dimensions
 - incorrect allowances
 - deformed pattern
 - pattern mounting error

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7. Inclusions
 - nonmetallic particles usually
 - bad for casting - acts as stress raiser
 - materials from alloys, crucible ,mold etc
 - sand particles, ceramic particles,
 - Can be avoided using filters, good strong molds etc

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BLOW HOLES

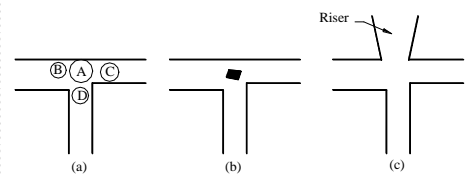
- Appears as small round voids opened to the casting surface.
- Caused by hard ramming and low permeability sands.

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SHRINKAGE DEFECTS

- Caused by inadequate feeding of molten metal.



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HOT TEARS

- Appears as external cracks or discontinuities on casting surface.
- Caused by hard ramming, too much of shrinkage of molten metal and poor design of casting.

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MISRUNS

- ❑ Mould cavity remaining unfilled (casting is too thin or temperature is too cold)

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












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- ❑ COLD SHUT
 - ❑ Imperfect fusion of molten metal in the mould cavity.
- ❑ POUR SHORT
 - ❑ Mould cavity is not completely filled for the want of molten material.
- ❑ INCLUSIONS
 - ❑ Foreign material present within the metal of a casting.

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Slide 54

Common Casting defects

 Blow	 Scar	 Blister	 Gas holes	 Pin holes
 Porosity	 Drop	 Dirt	 Buckle	 Scab
 Rat tail	 Penetration	 Swell	 Misrun	

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Common Casting defects

The slide displays seven diagrams illustrating common casting defects:

- Nonmetallic inclusion:** A cross-section of a casting with a region labeled 'Dross' and 'Nonmetallic inclusion'.
- Cold shut:** A cross-section of a casting with two regions labeled 'Gate' and a jagged interface between them.
- Shrinkage cavity:** A cross-section of a casting with a concave surface and a cavity below it.
- Wash:** A cross-section of a casting with a 'Gate' and a surface defect labeled 'Wash'.
- Hot tear:** A cross-section of a casting with a jagged fracture line labeled 'Hot tear'.
- Mold shift:** A circular cross-section of a casting with a distorted shape labeled 'Mold shift'.
- Core shift:** A circular cross-section of a casting with a distorted shape labeled 'Core shift'.

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Casting defects

The slide shows two photographs of casting defects:

- Left photograph:** A large gray iron valve body with a visible crossjoint.
- Right photograph:** A cross-section of spheroidal graphite cast iron showing inclusions.

- A crossjoint in a large gray iron valve body casting produced by mismatch of top and bottom parts of the mould
- Inclusions in spheroidal graphite cast iron.
- Part of the surface has been machined away to show the inclusions more clearly

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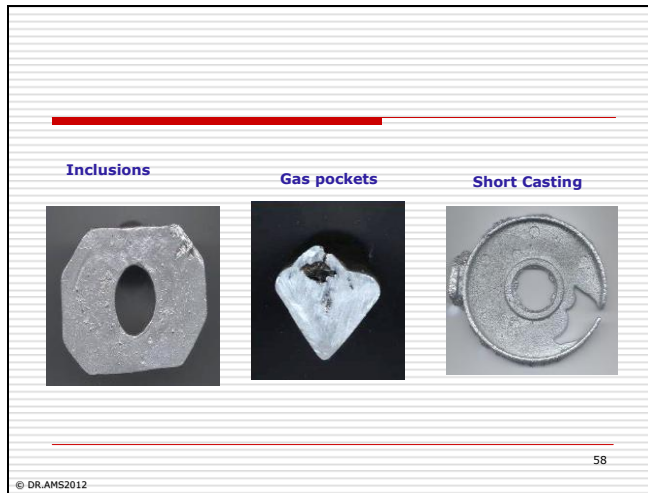
Flash **Mold Shift** **Porosity**

The slide displays three photographs of casting defects:

- Flash:** A casting with excess material on its edges.
- Mold Shift:** A casting with a distorted shape.
- Porosity:** A casting with a porous, irregular surface.

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Summary of casting defects

Defect	Cause	Foundry remedy	Design remedy
Flash	Flow into mold join	Lower pouring temperature, Increase mold box clamping.	
Oxide and dross inclusion	Entrapment of foreign material	Increase care and cleanliness during pouring.	
Shrinkage cavities	Lack of sufficient feed metal	Promote directional solidification by controlling heat flow, Raise pouring temperature.	Relocate risers and ingates
Misruns	Low metal fluidity	Raise pouring temperature	Reconsider position, size and number of ingates and vents

Slide 60

- ### Inspection of casting
1. Visual Inspection
 - Most surface defects can be seen
 2. Pressure test
 - The casting is filled with pressurized air after closing all the openings
 - E.g. gear boxes, pressure vessels, look for leaks by submerging in special liquids
 - Pressurized oil can also be used in some cases
 3. Radiographic Examination
 - Usually x-rays or g rays
 - x-ray method is used for voids, non metallic inclusions, porosity, cracks
 - Defects appear darker than surrounding

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4. Ultrasound examination

- Ultrasound across the casting
- Sound transmitted across homogenous metals
- However discontinuities reflect sound back.
- Not good for cast iron

5. Dye Penetration Inspection

- To detect invisible surface defects in non magnetic castings
- A dye of fluorescent material is sprayed or applied near the surface. The surface is then wiped and viewed in darkness
- Cracks will be visible

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6. Magnetic Particle inspection

- Induce magnetic field through section under inspection
- Powdered Ferro-magnetic material is spread onto the surface
- Voids or cracks result in abrupt changes in permeability of material - leads to leakage in magnetic field
- Particles concentrate on the disrupted field or on the crack.

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ADVANTAGES OF CASTING PROCESS

- No restriction on type of metal or alloy.
- No restriction on size of the component that can be casted.
- Economically suitable for batch and mass production.

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DISADVANTAGES OF CASTING PROCESS

- High energy consuming process.
- Highly labor intensive.
- Raw material requirement is quite high.
- For producing 1 ton of steel casting about 2.2 tons of metal, 0.3 tons of facing sand and 4 tons of baking sand are needed apart from many other materials.
- More time is involved.
- High environmental pollution.

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SELECTION OF CASTING PROCESS

- Quantity to be produced.
- Requirement of the product in terms of surface finish, accuracy, complexity etc.
- Physical properties of the material.
- Process capability to meet the requirement of point 2 and 3.
- Initial investment required and operational costs.
- Other factors such as environmental pollution, availability of skilled operator (if required), possibility of automation.

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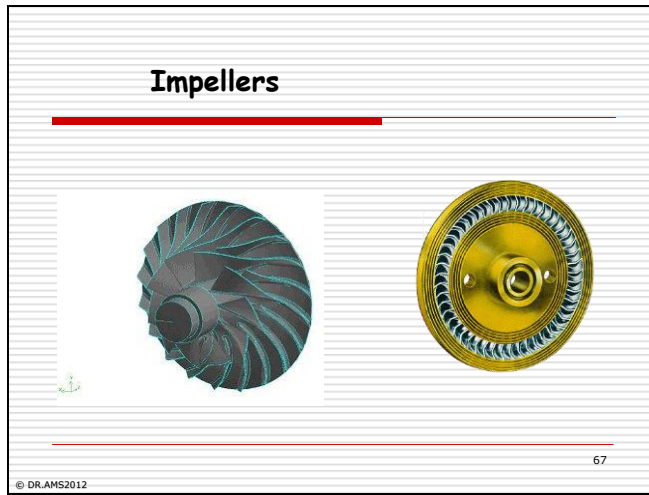
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Crank Shaft

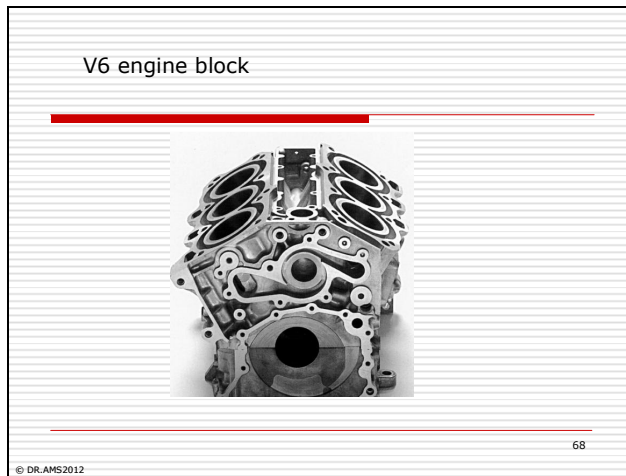


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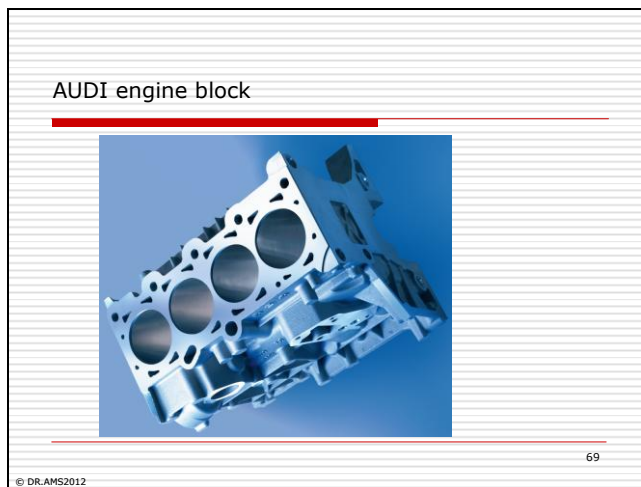
Slide 67



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EXAMPLE 1

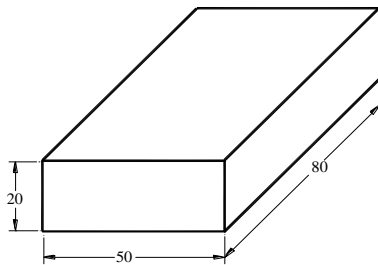
- A job shown in the Figure is to be made of steel by casting process. The mould for this job is made from a wooden pattern. Determine the dimensions of the wooden pattern. Assume machining allowance of 2 mm on each side, shrinkage allowance of 2% and a taper allowance of 1 degree.

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EXAMPLE -1



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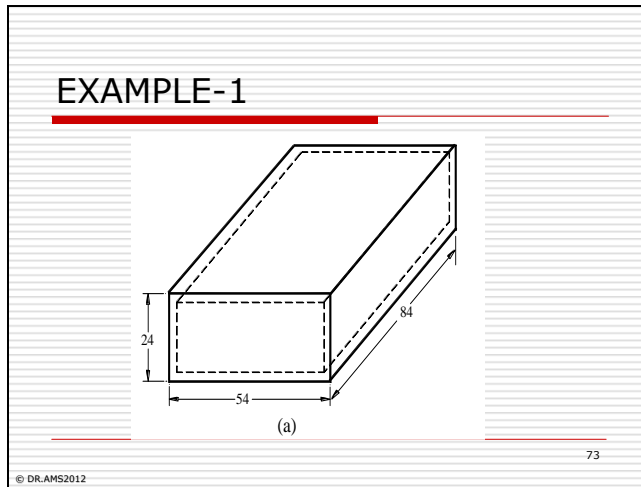
EXAMPLE-1

- **Solution**
- **Step-1: Machining Allowance**
- It is given that machining allowance of 2 mm on each side is to be given. Thus, each side is increased by 2 mm resulting in the basic dimension of the pattern as shown in Figure (a). The required casting is shown with dotted lines.

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EXAMPLE-1

- **Step-2 : Taper Allowance**
- We decide to cast the job horizontally and use a solid pattern for this casting. For this design, the draft allowance is to be provided on the vertical sides (24 mm long). Considering the given taper allowance of 1 degree, the side view of the pattern would be as shown in Figure (b).

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EXAMPLE-1

- The taper allowance value x is calculated from the geometry of the Figure (b) as
- $x = 24 \tan 1 = 0.419 \text{ mm.}$
- Thus, the top surface dimension is increased to provide for draft allowance from $54 \times 84 \text{ mm}$ to $54.838 \times 84.838 \text{ mm.}$

(b)

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Step-3 Shrinkage Allowance:

Given shrinkage allowance is 2%. Now, the dimensions of pattern are increased by 2% on all sides.

That is, dimension 54 mm will become

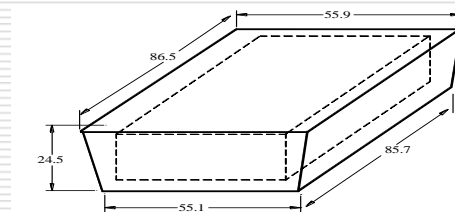
$$54 + (54 \times 2) / 100 = 55.08 \text{ mm or } 55.1 \text{ mm}$$

The dimension 54.838 will become

$$54.838 + (54.838 \times 2) / 100 = 55.9 \text{ mm}$$

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- Similarly, all other dimensions are calculated and the final dimensions of the pattern are shown in Figure

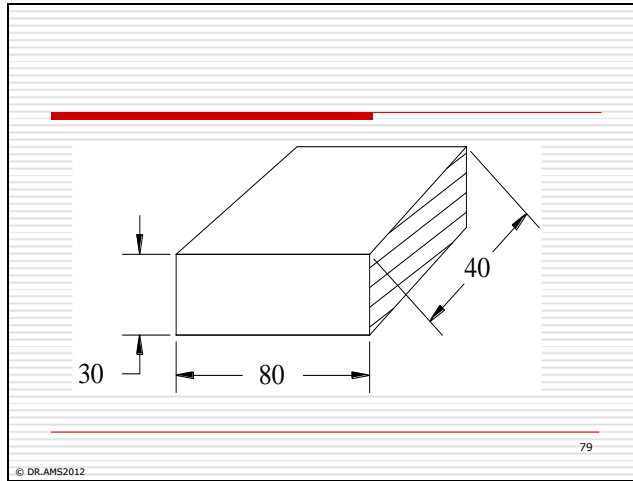


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□ **Example 2**

- A job shown in Figure 2 is to be made from steel by casting process. The mold for this job is made from wooden pattern. Determine the dimensions of the wooden pattern assuming machining allowance of 3 mm on each side, shaking allowance of 1 mm on length and width, shrinkage allowance of 3%

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□ **Solution**

□ **Step-1 : Machining Allowance**

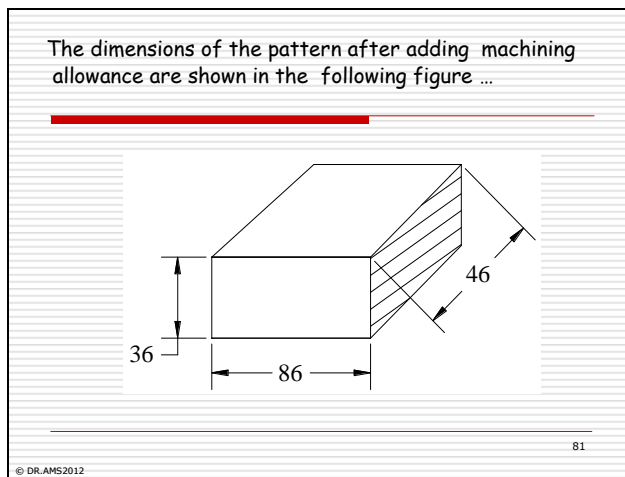
□ Since given machining allowance is 3 mm on each side, add 3 mm on each side of the part shown in Figure. The dimensions of the pattern after machining allowance will be:

- $L = 80 + 2 \times 3 = 86 \text{ mm}$
- $W = 40 + 2 \times 3 = 46 \text{ mm}$
- $H = 30 + 2 \times 3 = 36 \text{ mm}$

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Step-2 : shrinkage allowance

- The shrinkage allowance of 3% is added to all the dimensions of the pattern shown in Figure. Dimension of the pattern after providing shrinkage allowance of 3% will be:

- $L = 86 + 86 \times 3/100 = 88.58$ mm,
- $W = 46 + 46 \times 3/100 = 47.38$ mm
- $H = 36 + 36 \times 3/100 = 37.08$ mm

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EXAMPLE #2

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Step -3 : Shaking Allowance

- Given shaking allowance is 1 mm on length and width.
- Recall that, shaking allowance is a negative allowance.
- Hence, 1 mm has to be reduced from the calculated values of length and width side.
- Students are advised to note that the height of the pattern doesn't require any shaking allowance.

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EXAMPLE #2

□ Therefore, final dimension of the pattern will be:

- $L = 88.58 - 1 = 87.58 \text{ mm}$
- $W = 47.38 - 1 = 46.38 \text{ mm}$
- $H = 37.08 \text{ mm}$

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EXAMPLE #2

A 3D perspective drawing of a rectangular pattern. The dimensions are labeled: the length of the top edge is 87.58, the width of the bottom edge is 46.38, and the height of the vertical edge is 37.08. Arrows point to each dimension line.

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Example 3

The downsprue leading into the runner of a certain mold has a length = 175 mm. The cross-sectional area at the base of the sprue is 400 mm². The mold cavity has a volume = 0.001 m³. Determine: (a) the velocity of the molten metal flowing through the base of the downsprue, (b) the volumetric flow rate, and (c) the time required to fill the mold cavity.

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Example 3: Solution

- (a) **Velocity** $v = (2gh)^{0.5}$
 $= (2 \times 9810 \times 175)^{0.5}$
 $= 1853 \text{ mm/s}$
- (b) **Volume flow rate** $Q = vA$
 $= 1853 \times 400$
 $= 741,200 \text{ mm}^3/\text{s}$
- (c) **Time to fill cavity** $MFT = V/Q$

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Example 4

In casting experiments performed using a titanium alloy and a zircon sand mold, it took 155 s for a cube-shaped casting to solidify. The cube was 50 mm on a side. If the same alloy and mold type were used, find the total solidification time for a cylindrical casting in which the diameter = 30 mm and length = 50 mm.

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Example 4: Solution

□ Cube Volume V $= (50)^3$ $= 125,000 \text{ mm}^3$	• Cylinder Volume V $= \pi D^2 L / 4 = \pi (30)^2 (50) / 4$ $= 35,343 \text{ mm}^3$
□ Cube Area A $= 6 \times (50)^2$ $= 15,000 \text{ mm}^2$	• Cylinder Area A $= 2\pi D^2 / 4 + \pi DL$ $= \pi (30)^2 / 2 + \pi (30)(50)$ $= 6126 \text{ mm}^2$
□ Cube (V/A) $= 125,000 / 15,000$ $= 8.33 \text{ mm}$	• Cylinder (V/A) $= 35,343 / 6126$ $= 5.77 \text{ mm}$
□ $C_m = TST / (V/A)^2$ $= 155 / (8.33)^2$ $= 2.23 \text{ s/mm}^2$	• $TST = C_m (V/A)^2$ $= 2.23 (5.77)^2 = 74.3 \text{ s}$

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Example 5

A mold cavity has the shape of a cube, 100 mm on a side. Determine the volume and dimensions of the final cube after cooling to room temperature if the cast metal is copper. Assume that the mold is full at the start of solidification and that shrinkage occurs uniformly in all directions. For copper, solidification shrinkage is 4.9%, solid contraction during cooling is 7.5%.

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Example 5: Solution

- Volume of cavity V
 - = $(100)^3$
 - = 10^6 mm^3
- Volume of casting V
 - = $10^6(1-0.049)(1-0.075)$
 - = **$879,675 \text{ mm}^3$**
- Dimension on each side of cube
 - = $(879,675)^{0.333}$
 - = **95.82 mm**

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